333-125 AU 252 48764

WO 8702186 APR 1987

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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 4 : H01P 5/12, 1/162	A1	(11) International Publication Number: WO 87/02186 (43) International Publication Date: 9 April 1987 (09.04.87)

(21) International Application Number: PCT/US86/01934

(22) International Filing Date: 17 September 1986 (17.09.86)

(31) Priority Application Number: 783,593

(32) Priority Date: 3 October 1985 (03.10.85)

(33) Priority Country: US

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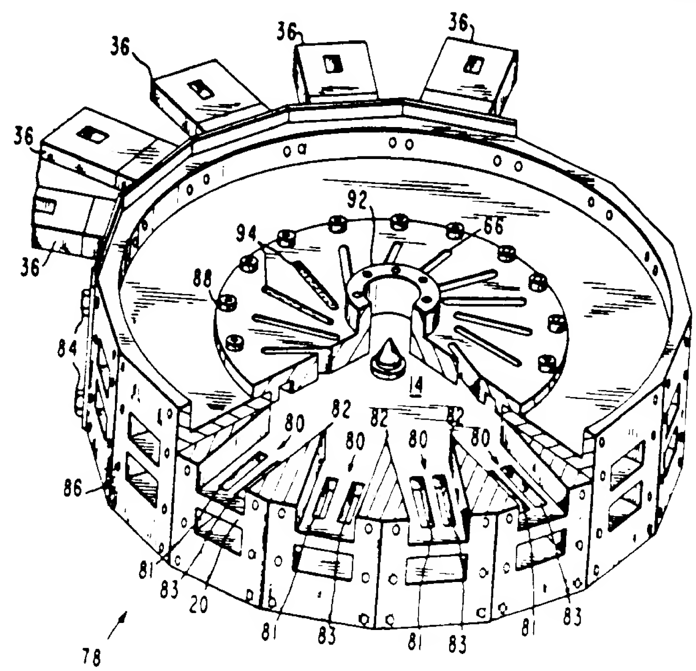
(81) Designated States: CH (European patent), DE (European patent), FR (European patent), GB (European patent), IT (European patent), JP, NL (European patent), NO, SE (European patent).

Published

With international search report.
Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.

(54) Title: NON-REACTIVE RADIAL LINE POWER DIVIDER/COMBINER WITH INTEGRAL MODE FILTERS



(57) Abstract

A parallel plate radial transmission line (14) having parallel plate spacing of less than $\lambda/2$ and which utilizes a specific higher order mode, preferably the first higher order circumferential mode. Undesired modes are suppressed by mode suppression slots (66) formed in one or both of the parallel plates and which are oriented parallel to the current flow lines (68) of the particular mode that is used. These slots (66) have a negligible effect on the mode being used but they couple out other modes that are generated by means such as by imperfections and imbalances in any active devices (36) coupled to the radial line. A centrally located feed is used to launch circularly polarized energy of the TE mode in the particular circumferential mode in the radial line (14). The feed may also receive circularly polarized energy of the particular circumferential mode in the radial line, linearly polarize that received energy

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NON-REACTIVE RADIAL LINE POWER DIVIDER/COMBINER WITH INTEGRAL MODE FILTERS

BACKGROUND OF THE INVENTION

The invention relates generally to parallel plate radial line devices and more particularly, to non-reactive devices with mode filters.

Conventional power divider/combiners use branching transmission line networks that start from a single input port and branch out to N output ports (where N is the number of such ports) and vice versa for a combiner. Such networks are commonly known as corporate feeds. A corporate feed that uses simple three port T-junctions at each branch point is known as a reactive feed. As is well known, a three port junction is not impedance matched looking into all ports, (see Montgomery, Purcell and Dicke, MIT Rad. Lab. Series Vol. 8, Principles of Microwave Circuits, Chapter 9), hence, spurious reflections from any source such as at any other junction, connectors, bends etc. within the corporate feed or from any device at any of the outputs can cause large errors in the output amplitudes and phases and can cause resonances within the feed network. As a result, it can cause undesirable mutual coupling between the output devices, such as amplifiers, to result in spurious reflections or oscillations and high power breakdown. If each simple three port T-junction were replaced by a matched four port hybrid such as a magic-T or quadrature hybrid, these problems would be greatly alleviated

because the spurious reflections are absorbed in the matched loads in the fourth port of the hybrid junction (see R. C. Johnson and H. Jasik, Antenna Engineering Handbook, Second Edition, pp. 20-55 through 20-56 and pg. 40-18).

A corporate feed using the above-described hybrid arrangement is typically quite complex, large, and costly because it contains on the order of N-1 hybrids, N-1 terminating loads, 2(N-1) bends and interconnecting transmission lines. It is also relatively lossy because, for cost purposes, the corporate feed is usually designed in stripline or microstrip which are very lossy compared to waveguide. Also, stripline and microstrip have not been able to handle high peak or high average powers.

The radial line power combiner is a type of non-reactive combiner for combining the outputs of a plurality of circumferentially mounted power sources in a single combining structure. Likewise, it is usable for dividing an input signal into a plurality of output signals in a single structure. By using two radial lines, one functioning as a power divider and the other as a power combiner, a high power transmitter may be formed by coupling a plurality of individual power amplifying devices to the circumferences of both radial lines. However, in prior radial line techniques, the failure of an amplifier or amplifiers or the mismatching of a part of the radial line causes the generation of higher order modes with a decrease in radial line efficiency and power output.

A prior technique used to suppress higher order modes in a radial line involves mounting resistors at the circumference of the radial line between the power sources. This technique is difficult to implement at the higher frequencies such as millimeter wave where

spacing of the coaxial probes into the radial line and proper positioning from the shorting cylinder that short circuits the parallel plates (see U.S. Patent 3,290,682, J. S. Ajioka, "A Multiple Beam Antenna Apparatus," December 1966).

In accordance with the invention, a higher order circumferential mode is used, preferably the first higher order mode. In the radial line functioning as a power divider an input waveguide feed centrally located in one of the parallel plates is used to launch circularly polarized TE_{11} ($|m|=1$) mode ($m=+1$ for a left hand circularly polarized wave and $m=-1$ for a right hand circularly polarized wave) in a circular waveguide which, in turn, launches the $m=\pm1$ mode in the radial line.

Mode suppression slots are formed in one or both parallel plates of the radial line for coupling undesired modes out. In the preferred embodiment, absorptive material is placed in or behind the slots to dissipate any such coupled power. In the principle of the invention, a mode of any order can be used and all other modes are suppressed by the slots formed in the parallel plate or plates of the radial line. The slots are oriented parallel to the current flow lines of the particular mode that is used and will have a negligible effect on that particular mode but will couple out others. The mode suppressing slots couple the spurious reflections mentioned above to the absorptive material to result in the electrical equivalent of a non-reactive corporate feed in which every junction is a matched hybrid.

In the radial line functioning as a power combiner in accordance with the invention, power input from positions on the circumference of the radial line is combined at a waveguide centrally located in one of the

the resistor size is small, thus making it difficult to handle. Also the use of a discrete resistor may limit the power handling capabilty of the radial line.

Accordingly, it is an object of the invention to provide a radial line power divider/combiner which has the advantages of a radial line and which suppresses undesirable modes.

It is also an object of the invention to provide a radial line power divider/combiner which is able to handle relatively large power levels more efficiently.

SUMMARY OF THE INVENTION

The above objects and other objects are attained by the invention wherein there is provided a parallel plate, radial line power divider/combiner which, as a divider, has a means for launching circularly polarized, higher order mode energy through a centrally located port in the radial line, and has mode suppressing slots formed in one or both parallel plates of the radial line with associated absorption material for suppressing undesired modes. As a combiner, the radial line also has such mode suppressing slots formed in one or both parallel plates of the radial line and also has associated absorption material for suppressing undesired modes. Furthermore, the power combiner radial line has a centrally located means for coupling out the combined higher order mode power. Where required, a transformer, such as an annular groove, is used to impedance match the cylindrical waves of the radial line to an array of output waveguides or other coupling device at the circumference. If coaxial lines are used as the circumferential output ports of the radial line, the annular groove transformer is not necessary since impedance matching can be achieved with proper

parallel plates which couples the combined, higher order mode energy to a circular polarizer. Mode suppression slots are also formed in one or both parallel plates of the radial line parallel to the current flow lines of the desired mode.

A radial line power divider/combiner is a traveling wave (non-resonant) combiner. In accordance with the invention, it utilizes a higher order circumferential mode, perferably the first higher order mode ($|m|=1$). The mathematical form for cylindrical modes in the radial line is $e^{\pm jm\phi} H_m^{\{1 \atop 2\}}(kr)$ where $e^{\pm jm\phi}$ indicates the circumferential phase progression and $H_m^{(2)}(kr)$ defines the outward radiating waves and $H_m^{(1)}(kr)$ defines the incoming waves (where H is the Hankel function, k is $2\pi/\lambda$ and r is the radial distance from the center). As discussed above, the mode suppression slots disposed in one or both parallel plates are oriented parallel to the current flow lines of the particular mode that is being used. The current flow lines are unique to each mode. To a very high degree of accuracy, the current flow lines for a given mode are straight lines tangential to an imaginary circle of m wavelengths in circumference having a center located on the center line of the feed waveguide where m is the mode used. In accordance with the invention, the mode suppressing slots are concidental with these tangential lines. It is a well known principle that narrow slots located parallel to the RF current flow lines have very little effect on the wave; however, if the RF current has a component perpendicular to the slot, an electric field is generated across the slot and the slot could radiate this energy out of the structure if allowed. (See MIT Rad. Lab Series Vol. 12 Microwave Antenna Theory and Design edited by S. Silver, p. 286, Sec. 9.9). By placing absorbing material in the slot or in the region behind the slot, the coupled energy is absorbed.

Thus, the invention provides a relatively low cost, low loss, high power, and compact non-reactive power divider/combiner. The mode suppression slots make it the electrical equivalent of a conventional corporate feed power divider/combiner in which a four port hybrid such as a magic tee is used at each branch point in the corporate feed.

BRIEF DESCRIPTION OF THE DRAWINGS

The various features and advantages of the invention together with further features, advantages and objects thereof are described with more precision in the following detailed description taken in conjunction with the accompanying drawings, in which:

FIG. 1a is a schematic, block diagram of a cross-sectional side view of two non-reactive radial line power divider/ combiners in accordance with the invention showing two parallel plate radial transmission lines both with circular waveguide feeds centrally located in one of the circular parallel plates, the feeds having circular polarizers and orthomode transducers, and also showing hybrid couplers, and amplifiers located at the circumferences of the radial transmission lines;

FIG. 1b is an enlarged view of a part of FIG. 1a presenting in greater detail the function of the couplers and amplifiers attached to the radial line power divider/combiners;

FIG. 2 is a rigorous computer plot of the mode cutoff circle, tangential current flow lines, and the equiphase contour which is shown as two spirals othogonal to the current flow lines;

FIGS. 3a and 3b are diagrams showing the orientation and shape of mode suppression slots in accordance with the invention where FIG. 3a is the opposite sense of FIG. 3b;

FIG. 4 is a partially cutaway perspective view of an embodiment of two non-reactive radial lines in accordance with the invention which have devices coupled at their circumferences to form a power amplifier. The radial lines, an input feed waveguide, circumferentially mounted waveguides having slots to form broadwall couplers, mode suppressing slots, and circumferential devices comprising directional couplers and amplifiers are shown; and

FIG. 5 is a top view of a radial line in accordance with the invention showing the placement of mode suppression slots, the mode cutoff circle and a plurality of processing devices coupled at the circumference.

DETAILED DESCRIPTION OF THE INVENTION

Referring now to the drawings wherein like reference numerals designate like or corresponding elements among the several views, there is shown in FIG. 1a a block diagram representation of a pair of m=1 mode radial line power divider/combiners 10 and 12 in accordance with the invention. The upper radial line 10 functions as a power divider in this embodiment and includes a radial transmission line 14 for dividing applied energy. The lower radial line 12 functions as a power combiner and includes a radial transmission line 16 for combining amplified energy in this embodiment. Each radial transmission line 14, 16 has two parallel plates (18, 20 and 22, 20 respectively) where parallel plate 20 is a common plate in this embodiment. Circularly polarized energy is launched into the power divider radial transmission line 14 by a suitable means such as by a waveguide 24 feed with an orthomode transducer 26 and a circular polarizer 28. In the invention, a higher order circumferential mode is used and the input waveguide 24

is dimensioned to support that mode. For example, where the preferred first order mode m=1 is used, a circular waveguide 24 dimensioned to support the TE_{11} mode is used. Energy 30 introduced into one port 32 of the orthomode transducer 26 is circularly polarized by the quarter wave plate circular polarizer 28, thus, the power divider radial transmission line 14 is circularly polarized. Energy introduced into the other port 33 of the orthomode transducer 26 would be circularly polarized in the opposite sense by the circular polarizer 28. A circular polarizer means usable in the invention may take the form of a quarter wave plate such as that shown or other types of circular polarizers known in the art.

As the relatively low power input energy 30 enters the power divider radial transmission line 14, it is divided equally around the radial transmission line 14 and is coupled to its circumference. In FIG. 1a, the matching device 34 may take the form of a conical object as shown or other shape. Also, other types of matching devices such as a tuning "button" known in the art may be usable.

In FIGS. 1a and 1b, there are shown in block form, amplifiers 36 and directional couplers 38 coupled to the radial transmission lines 14 and 16 at their circumferences. The amplifiers 36 may be of a reflective type and the directional couplers 38 may be of a type known in the art as 3 dB hybrid couplers. Shown in FIGS. 1a and 1b are 3 dB topwall hybrid couplers 38 which have two slots in a septum (one slot 40 is shown). As is known in the art, the size of the slots is chosen to achieve the amount of coupling desired. The couplers 38 shown are used in the embodiments of FIGS. 1a, 1b and 4 where there are two amplifiers 36 located at each circumferential position. Where a different

arrangement is required, a different type of coupler may be used. In some applications, such as shown in FIG. 5, no coupler whatsoever may be required and the amplifier or other circumferential processing device used may be coupled directly to the circumference of the radial transmission line, or, in another case, waveguides may be used between the radial transmission line and the circumferential processing device as shown in FIG. 4.

Where reflective amplifiers are used, as the amplifiers 36 shown in FIGS. 1a, 1b, and 4, the incident low power enters the amplifier input/output port and the amplified high power leaves this same port; hence, it is equivalent to a reflection with a reflection coefficient greater than unity. Therefore, if two identical amplifiers 36 were coupled to two ports 42, 44 of a 3 dB hybrid directional coupler 38 as shown in FIG. 1b, the incident low power entering the hybrid coupler 38 through its input port 46 will be split in half (3 dB), input to both amplifiers 36 through the hybrid coupler amplifier ports 42, 44 and be reflected (with a reflection coefficient greater than unity--the gain of an amplifier) at each of the same ports 42, 44. Due to the nature of the hybrid coupler 38, these reflections will add in phase at its output port 48 and will cancel in phase at its input port 46 thereby causing the amplified power outputs of the amplifiers 36 to enter the combining radial transmission line 16 where they are combined in phase at the centrally located waveguide 50 feed. As used herein, a feed is a means for conducting power to or from the radial line power divider/combiner. Commercially available broadwall hybrid couplers are suited for use as the directional coupler 38 described above.

The power combined in the power combiner radial transmission line 16 which is circularly polarized is converted to linearly polarized energy 52 by the circular polarizer 54 which is coupled to the output waveguide 50 feed, and appears at one of the ports 56 of the orthomode transducer 58 also coupled to the output waveguide 50 feed. Any residual power that is of the undesired oppositely rotating mode will appear in the orthogonal port 60 of the orthomode transducer 58 and can be absorbed by attaching a terminating load 62. The circular polarizer 54 used here may be the same type as that used in the power divider radial line 10. The output waveguide 50 feed is also dimensioned to support the desired mode, preferably the TE_{11} mode.

In this embodiment shown in FIG. 1a, the power divider radial transmission line 14 is identical to the power combiner radial transmission line 16. Thus, a relatively low power input signal 30 is amplified and output as a relatively high power output signal 52 through the use of two "back-to-back" radial transmission lines 14 and 16 and amplifying processing means 38, 36 coupled to their circumferences. Also shown in FIGS. 1a and 4 are annular impedance matching grooves 64. These grooves 64 match the waves of the radial transmission lines 14, 16 to the directional couplers 38. Such matching means may not be required such as where coaxial probes are used instead of waveguide directional couplers. Matching is then accomplished by positioning the coaxial probes appropriately.

Imbalances in phase and/or amplitude among the amplifiers 36 (which are ideally identical) typically generate undesired modes in the radial line which can cause high coupling between the amplifiers 36 which, in turn, can cause spurious oscillation and damage to the amplifiers 36. As part of the invention, mode suppression

slots are provided in one or both parallel plates of the radial transmission line. The mode suppression slots will couple out the power in the undesired modes into an absorption means and the desired isolation between amplifiers 36 will be maintained. A common situation is where an amplifier fails. This failure typically generates a large number of undesired modes which can lead to the catastrophic results explained above. The mode suppression slots will perform as described to maintain isolation between the remaining amplifiers and allow continued operation.

Such mode suppression slots 66 are shown in FIGS. 3a, 3b, 4, and 5. They are oriented parallel to the current flow lines of the particular mode used. Since narrow slots have a negligible effect on parallel currents as discussed above but couple perpendicular components, the particular mode used will be affected very little by the parallel slots 66 while other modes will be coupled out of the radial transmission line. The inventor has found that the current flow lines for any particular circumferential mode are straight lines tangential to a mode cutoff circle which is a circle of "m" wavelengths in circumference, where m is the mode number, i.e., there are $m2\pi$ radians of phase change in going around the mode cutoff circle of a circumferential mode.

A rigorous computer plot of current flow lines 68 for the m=1 mode are shown in FIG. 2. The mode cutoff circle 70 is an imaginary circle of m-wavelengths in circumference and is called such because it has been found that the mode is cut off and does not propagate inside the circle 70. It may also be called the mode caustic circle because incoming rays (which are identical to the current flow lines 68) are tangent to this

circle 70 which defines a caustic curve in geometrical optics. In FIG. 2, the numeral 68 has been used to point out only a few of the current flow lines to maintain clarity.

For +m, the tangential current flow lines are of one sense and for -m, the lines are of the opposite sense. A single sense is shown in FIG. 2 however FIGS. 3a and 3b which will be discussed in greater detail below, present both senses. It has also been found that constant phase contours 72 are orthogonal trajectories to the current flow lines 68 and form a spiral, the lines of which are spaced $m2\pi$ radians apart, as shown in FIG. 2 (two spirals 72 are shown). It is also interesting to note that the power flow lines (Poynting vector, $\overline{S} = \overline{E} \times \overline{H}$) are the same as the current flow lines 68 ($\overline{J} = \hat{n} \times H$) where $\hat{n}$ is the unit normal vector to the plates) and since $\hat{n}$ and $\overline{E}$ are both normal to the plates, $\overline{S}$ and $\overline{J}$ are parallel. Thus constant phase contours 72 are normal to the power flow lines. The precise angle of the current flow lines 68 with respect to a radius is believed to be given by:

$$\tan\alpha = \frac{J_\phi}{J_n} = \frac{H_r}{H_\phi} = \frac{jm\lambda}{2\pi r}\,\frac{H_m^{(2)'}(kr)}{H_m^{(2)}(kr)}$$

where

J_ϕ = component of current in the ϕ-direction

J_r = radial component of current

H_r = radial component of the magnetic field

H_ϕ = ϕ-component of the magnetic field

m = the mode number

r = radial distance from the origin

$k = \frac{2\pi}{\lambda}$

$H_m^{(2)}(kr)$ is the Hankel function corresponding outward traveling waves,

$H_m^{(2)'}(kr)$ is the derivative of $H_m^{(2)}(kr)$ with respect to its argument kr.

It has been found that to a very high degree of accuracy, tan α is a real constant and equal to the geometrical tangents to a circle of m-wavelengths in circumference as shown in FIG. 2 (mode cutoff circle 70). Current distributions in waveguide usually given in the literature are a composite of +m and -m modes which are rather complex because they are interference patterns between the +m and -m current distributions. Mathematically,

$$e^{jm\phi} + e^{-jm\phi} = 2 \cos m\phi \text{ or}$$
$$e^{jm\phi} - e^{-jm\phi} = 2j \sin m\phi$$

where $\cos m\phi$ or $\sin m\phi$ are "standing wave" expressions in the ϕ-coordinate which is a combination $e^{+jm\phi}$ and $e^{-jm\phi}$, which are each "traveling wave" expressions of waves traveling in opposite directions in the ϕ-coordinate. Waves of equal amplitude traveling in opposite directions constitute a standing wave. Thus, the invention is directed to operation on the traveling wave, as opposed to prior techniques which operate on the standing wave.

A mode suppression slot arrangement in accordance with the invention is shown in FIGS. 3a and 3b. In one embodiment, such as where a radial transmission line in accordance with the invention is used as a power divider, both parallel plates would be slotted as is plate 74 in FIG. 3a. As is shown, the slots 66 are oriented such that they are coincidental with tangents to a

mode cutoff circle 70 (FIG. 2). Two types of slots are shown in FIGS. 3a and 3b, a continuous slot 66 and an interrupted slot 76. While these slots 66, 76 are shown as alternating, other embodiments are possible. These figures are not meant to be exhaustive of the types of slot configurations usable in the invention and other configurations are possible.

In FIG. 3a, slots of one sense are shown and in FIG. 3b, slots of the opposite sense are shown. Depending upon the direction of energy rotation in the radial transmission line, both parallel plates of the radial transmission line power divider in accordance with the invention may have slots oriented as in FIG. 3a. If the direction of rotation is opposite, both parallel plates would be slotted as in FIG. 3b. However, in the case where one parallel plate is common to two radial transmission lines and each radial transmission line conducts energy rotating with different senses, that common plate cannot be slotted as in either FIG. 3a or 3b since the energy of a sense having a component perpendicular to the slot will couple out of that radial line and into the other. Thus the common parallel plate is unslotted. This situation would apply to the embodiments shown in FIGS. 1a, 1b, and 4.

In the embodiments of FIGS. 1a, 1b, and 4, two "back-to-back" radial transmission lines 14, 16 are used to combine the power of N reflective type amplifiers 36 (where N = the number of amplifiers) such as IMPATT diode amplifiers or phase locked oscillators. One radial transmission line 14 divides and distributes the relatively low power input energy 30 to the N power amplifiers 36 and the other radial transmission line 16 combines the higher power output energy of the N amplifiers; hence, there is a relatively low power

divider and a relatively high power combiner with a common parallel plate 20. In this back-to-back embodiment, mode suppression slots 66 are formed only in the outer parallel plates 18, 22 which are not common to the two radial transmission lines 14, 16.

In FIG. 4 there is presented a perspective, partially cutaway view of an embodiment of the invention as a power divider/combiner 78 which functions as an amplifier. A microwave radial line power divider/combiner 78 is shown using two back-to-back parallel plate radial transmission lines as schematically shown in FIG. 1. In FIG. 4, the two radial transmission lines with circumferential waveguides 80 have been formed as a single structure. The vanes 82 are part of the structure and define the waveguides 80 to which the amplifiers 36 are coupled. In this embodiment, the waveguides 80 have been formed into 3 dB broadwall couplers such as that shown in FIG. 1 by forming two appropriate slots 81 and 83 in each waveguide region 80 of the parallel plate 20 which is common to both radial transmission lines. This allows the amplifiers 36 to be directly connected to these ports on the circumferences formed by the waveguides 80. As shown in FIG. 4, the amplifiers 36 are attached to the circumferences of the radial transmission lines and waveguides 80 by means of inserting screws 84 through the mounting flange of the amplifier 36 and into screw holes 86.

Also shown in FIG. 4 is a slotted plate 88 similar to those shown in FIGS. 3a and 3b which covers the radial transmission line 14. In the embodiment of FIG. 4, the slots 66 extend only over the radial line portion of the structure. In other embodiments, these slots 66 may continue over the waveguides 80 to provide continued

mode suppression. As shown in FIG. 5, the mode suppression slots 66 continue to the circumference of the radial transmission line 14 where a plurality of processing devices 90 are attached.

In the embodiment of FIG. 4, the slotted plate 88 is removable however this need not be the case. Also shown is an input circular waveguide and flange 92 to which an input signal power source may be connected. The size of the input waveguide is such that it supports the desired higher order mode and as such, is typically larger than the mode cutoff circle 70 (FIG. 2).

As previously discussed, FIG. 4 presents an embodiment where reflective amplifiers 36 are used. By using the 3 dB broadwall coupler formed by the two slots 81 and 83, two reflective amplifiers 36 are used at each circumferential position as shown more clearly in FIG. 1a. This arrangement has two advantages, the first is that twice as many amplifiers can be combined without enlarging the entire package and the second is that the hybrid arrangement alleviates the high isolation requirements of circulators which are normally associated with each amplifier in prior techniques and which may even be eliminated entirely. Although it has been described above that waveguide sections with 3 dB broadwall coupling slots can be used in an embodiment of the invention, they need not be used in other embodiments. However they have been found to have the advantages of low loss and high power handling capability.

Energy coupled out of the radial transmission line by the mode suppression slots may be absorbed by an RF lossy material. In FIG. 4, some of the mode suppression slots 66 are shown as being filled with an RF lossy material 94 such as Eccosorb made by Emerson & Cuming, Inc., having an address of Gardena, California 90248. The slotted plate 88 may also be painted with

Slots may be formed in both parallel plates of this radial line 14. Where reflections or oscillations are generated in the radial line 14, the mode suppression slots 66 will couple them out.

Modifications to the above description and illustrations of the invention may occur to those skilled in the art, however, it is the intention that the scope of the invention should include such modifications unless specifically limited by the claims.

an RF absorptive paint. Other means for absorbing the slot coupled energy or conducting it elsewhere may be used such as placing an RF lossy material 94 over the slots on the outer plates 18 and 22 as shown in FIG. 1a.

Thus, there has been disclosed a new and improved non-reactive radial line power divider/combiner. This radial line power divider/combiner has the advantages of radial transmission lines and due to the improvements of the invention, additionally suppresses undesired modes without degradation of its power handling capability. As is well known to those skilled in the art, an advantage of the radial line is the ability to adjust its size to accommodate an increase in the number of circumferentially mounted devices. The circumference of the radial line is merely enlarged to accommodate more devices.

Although the invention has been described and illustrated in detail, this is by way of example only and is not meant to be taken by way of limitation. For example, in FIGS. 1 and 4, the radial line is shown in an embodiment where there are two such radial lines joined by a common parallel plate 20 and having directional couplers 38 and reflective amplifiers 36 attached at the circumferences. Furthermore, FIG. 4 shows the use of waveguides between the radial line and the circumferentially attached directional couplers 38. Other embodiments of the invention are possible, such as that shown in FIG. 5 where a single radial transmission line 14 is used with circumferentially attached processing devices 90. These devices 90 may be amplifiers and their outputs may be conducted elsewhere as shown by the arrows 96. In this case, the radial line would function as a power divider with no waveguides or directional couplers between it and the amplifiers 90.

CLAIMS

In the claims:

1. A radial line power divider/combiner for processing applied energy comprising a radial transmission line (14) to which energy is applied and from which energy is output, the radial transmission line (14) comprising first and second parallel, circular, electrically conductive plates (18, 20) and having a centrally located feed, characterized in that:

the plates (18, 20) of the radial transmission line (14) are separated from each other by less than one-half of the wavelength of the applied energy;

the radial transmission line further comprises a circular feed port centrally located in one of the plates through which energy may be fed, the port being dimensioned to support a selected mode m where |m| is at least one;

a feed means for feeding the selected m circumferential mode, circularly polarized energy is coupled to the feed port for feeding the radial transmission line (14);

at least one slot (66) is formed in the parallel plates (18, 20), the at least one slot (66) oriented such that its longitudinal centerline is parallel to the current flow (68) of the selected m circumferential mode energy whereby the at least one slot suppresses modes other than the selected mode m from the energy output of the radial transmission line (14).

2. A radial line power divider/combiner according to Claim 1 characterized in that the feed means comprises:

a TE_{11} mode waveguide (24) coupled to the centrally located port through which the applied energy may be fed; and

a polarizing means (28) for polarizing the energy fed through the waveguide (24).

3. A radial line power divider/combiner according to any of the preceding claims characterized in that at least one slot (66) is formed in each of the plates (18,20), the slot (66) being oriented such that its longitudinal centerline is parallel to the current flow of the selected m circumferential mode energy whereby the slot (66) suppresses modes other than the selected m from the energy output of the radial transmission line.

4. A radial line power divider/combiner according to any of the preceding claims characterized in that the at least one slot (66) is oriented such that its longitudinal centerline is coincidental with a line (68) tangent to a circle (70) having a circumference substantially equal to the selected m wavelengths of the energy, the circle (70) having its center lying on the centerline of the centrally located port.

5. A radial line power divider/combiner according to any of the preceding claims characterized in that it further includes an absorption means (94) for absorbing energy coupled by the at least one slot (66).

6. A radial line power divider/combiner according to Claim 5 characterized in that the absorption means is disposed in the at least one slot (66).

7. A radial line power power divider/combiner according to any of the preceding claims characterized in

8. A radial line power divider/combiner according to Claim 7 characterized in that the second feed means comprises a second TE_{11} waveguide (50) coupled to the centrally located port of the second radial transmission line (16) for outputting the combined energy and linearly polarizing means (54) for linearly polaring energy conducted by the second waveguide (50).

9. A radial line power divider/combiner according to Claim 7 characterized in that the processing means comprises a plurality of amplifiers (36) to which the energy received from the first radial transmission line (14) is coupled by the processing means and from which the amplified energy is coupled to the circumference of the second radial transmission line (16) by the processing means.

10. A radial line power divider/combiner according to Claim 9 characterized in that:

the processing means comprises a plurality of unidirectional couplers (38) which are coupled to the circumferences of both radial transmission lines (14,16) and to the plurality of amplifiers (36) and which couple energy received at the circumference of the first radial line (14) substantially in one direction to the amplifiers (36) and which couple the amplified energy from the amplifiers (36) substantially in one direction to the second radial line at its circumference (16); and

the plurality of amplifiers (36) are disposed around the circumferences of the radial transmission lines (14,16) in such a way that there are two amplifiers at each circumference position.

that it further includes a second radial transmission line (16) comprising first and second parallel, circular, electrically conductive plates (22, 20) and has a centrally located feed, and is interconnected with the first radial transmission line (14) by circumferentially located coupling means, characterized in that:

the feed means of the first radial transmission line (14) includes a circular polarizer (28) for circularly polarizing the the applied energy, the feed means also launches the selected m circumferential mode, circularly polarized energy in the first radial transmission line (14) through the feed port;

the second radial transmission line includes at least one slot (66) formed in the parallel plates (22, 20), the at least one slot (66) oriented such that its longitudinal centerline is parallel to the current flow (68) of the selected m circumferential mode energy whereby the at least one slot suppresses modes other than the selected mode m from the energy output of the second radial transmission line (16);

the second radial transmission line includes a circular feed port centrally located in one of the plates through which energy may be fed, the port being dimensioned to support the selected mode m;

the coupling means includes a processing means for processing energy received from the first radial transmission line (14) at its circumference and applying the processed energy to the second radial transmission line at its circumference;

a second feed means is included for receiving the selected m circumferential mode, circularly polarized energy in the second radial transmission line combined at the centrally located feed port thereof and for linearly polarizing and outputting the combined, received energy.

Fig. 1a.

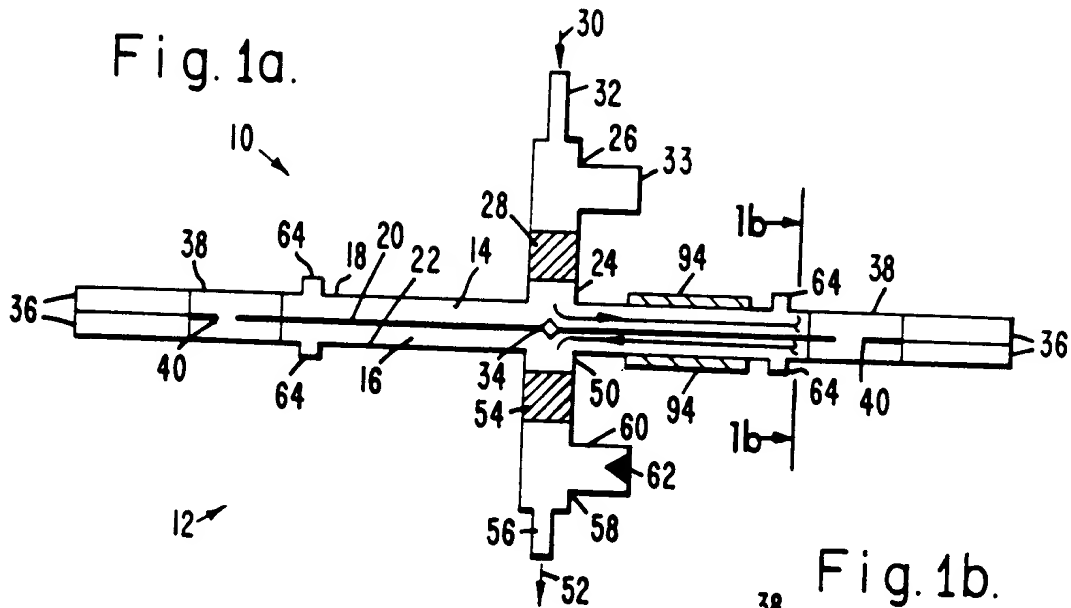
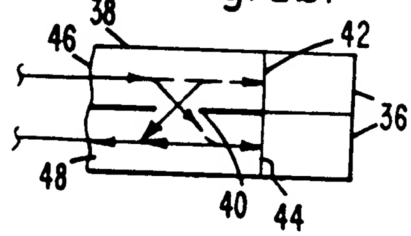


Fig. 1b.



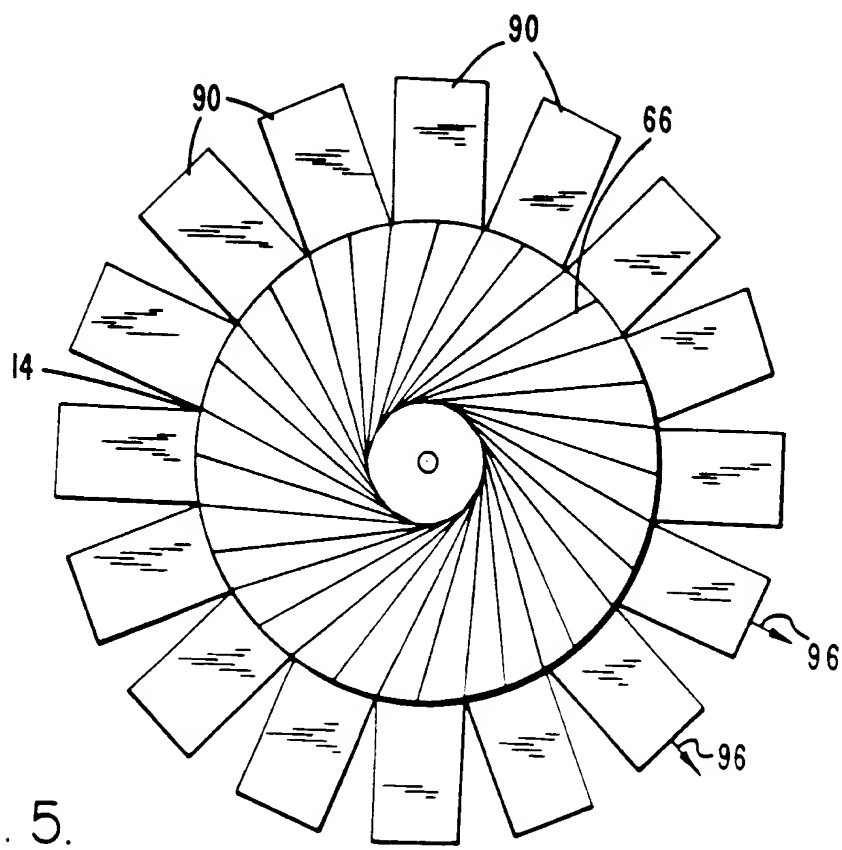


Fig. 5.

Fig. 2.

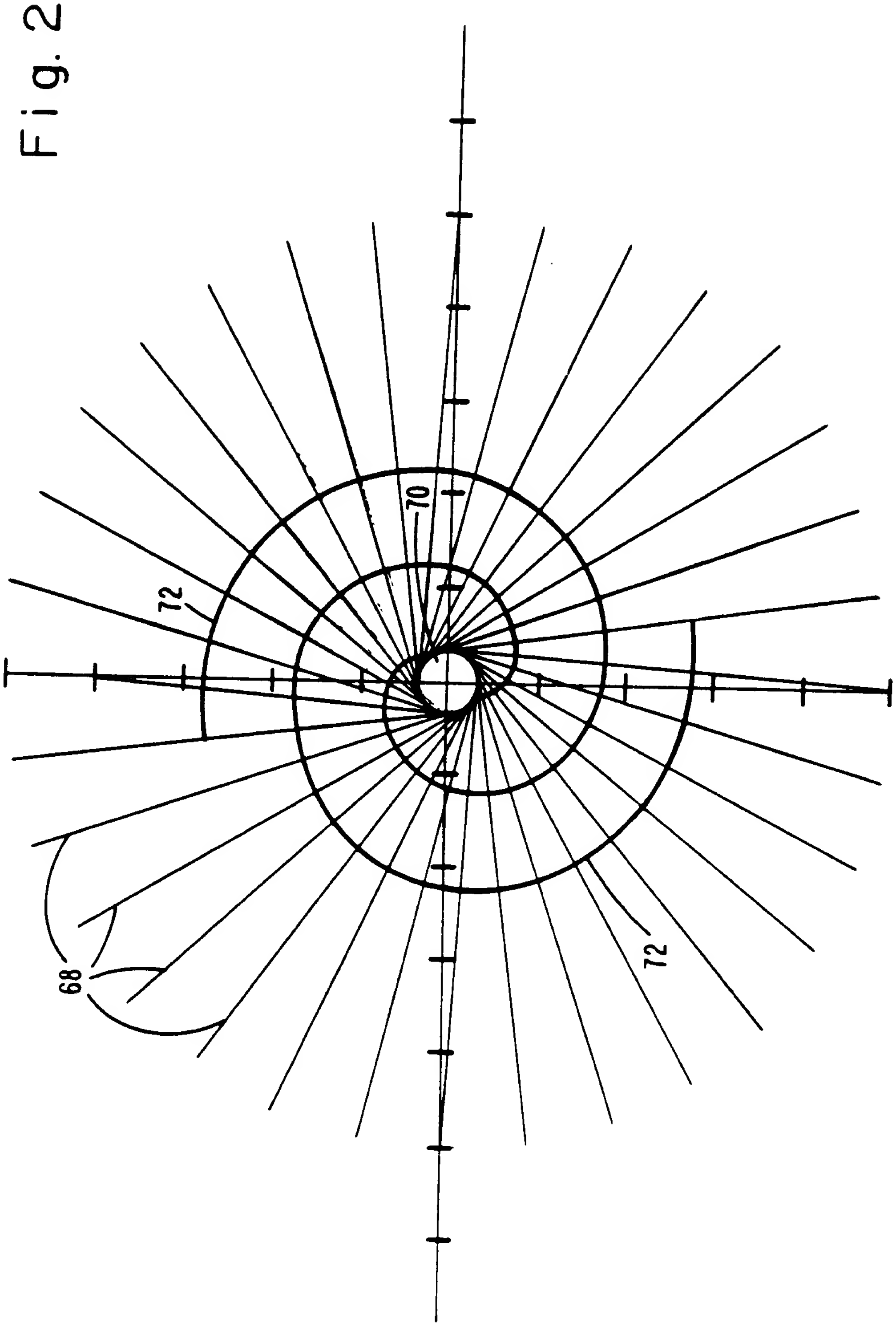


Fig. 3a.

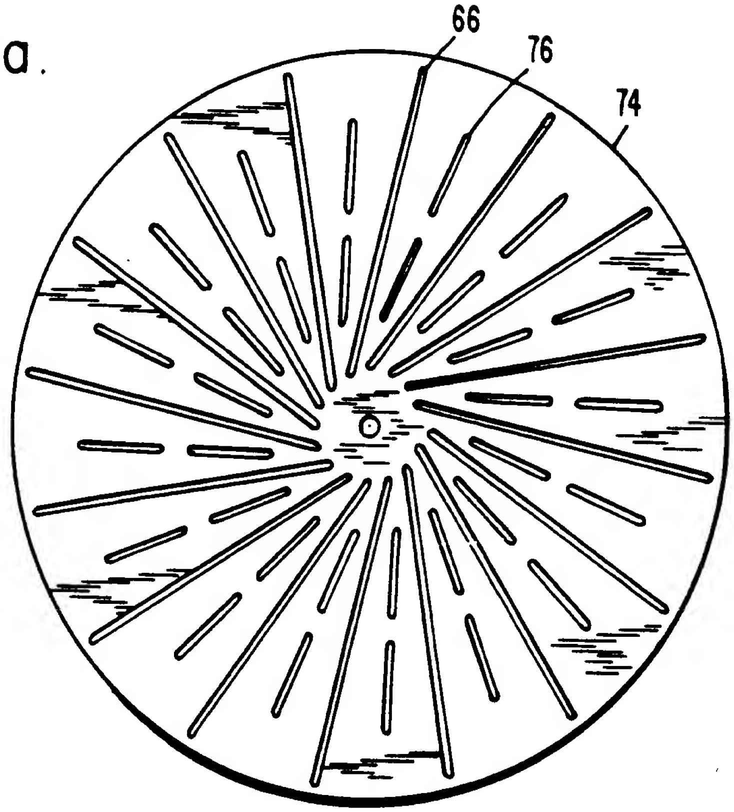
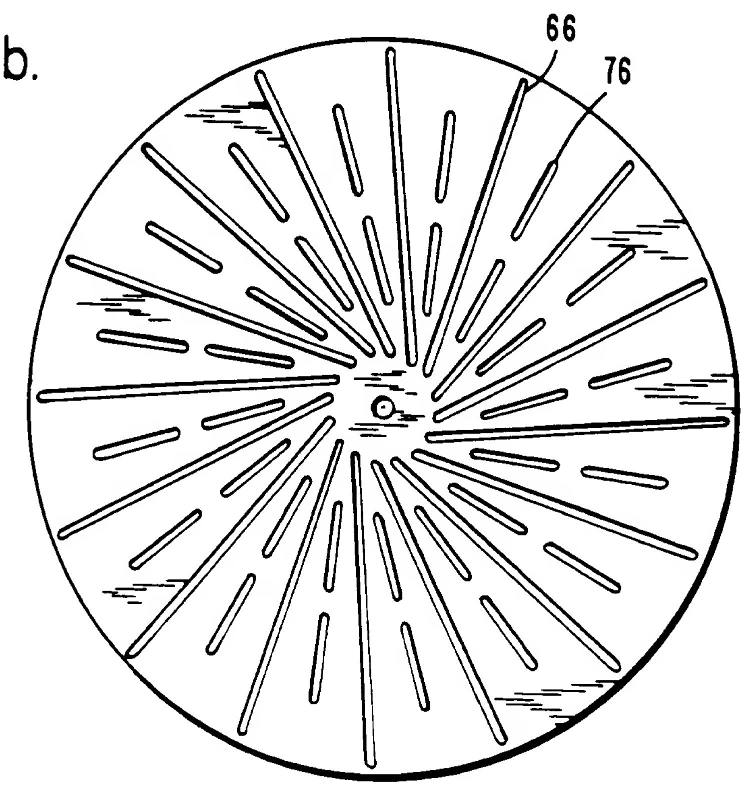


Fig. 3b.



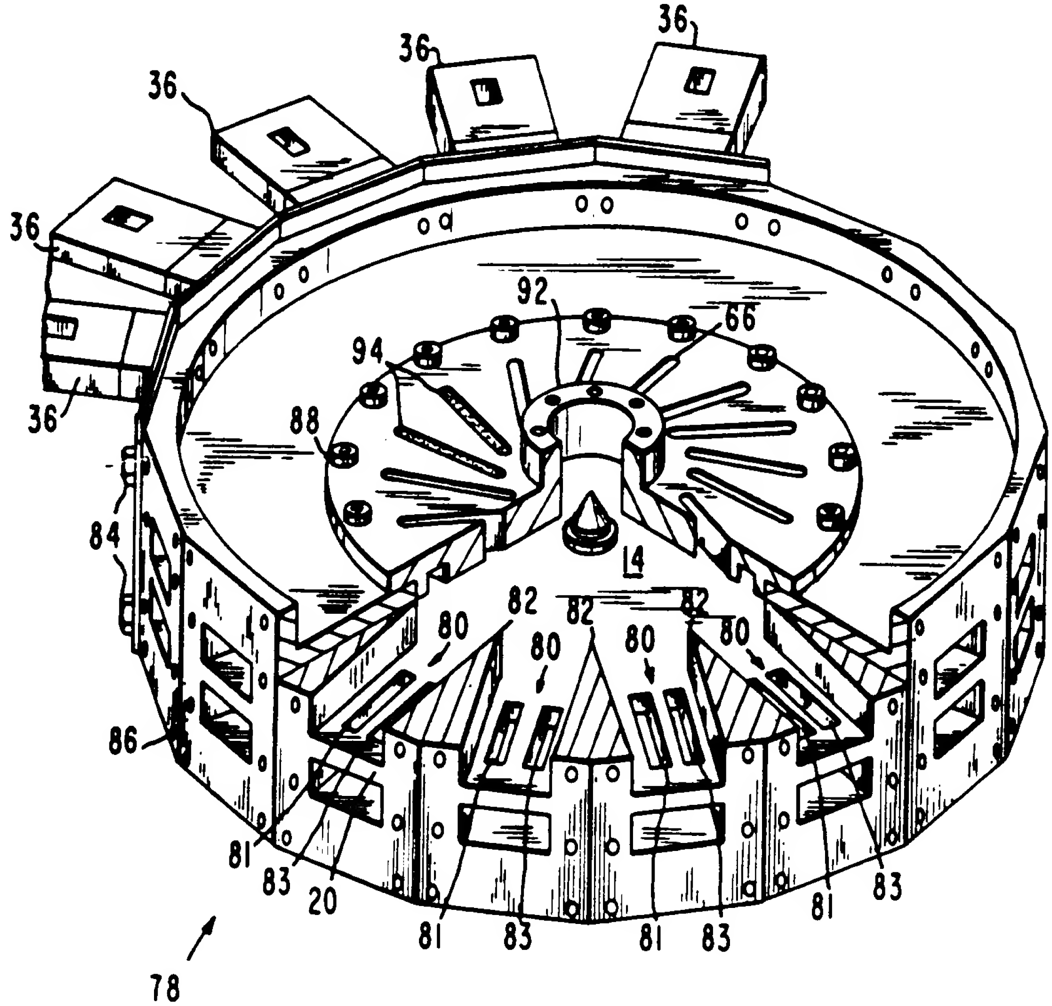

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Fig. 4

ANNEX TO THE INTERNATIONAL SEARCH REPORT ON

INTERNATIONAL APPLICATION NO. PCT/US 86/01934 (SA 15471)

This Annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 03/04/87

The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
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		GB-A-	990245	
		DE-A-	1298159	
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EP-A- 0020196	10/12/80	FR-A,B	2456399	05/12/80
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US-A- 2692977		None		
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GB-A- 887572		None		
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		GB-A-	2126816	28/03/84

For more details about this annex :
see Official Journal of the

INTERNATIONAL SEARCH REPORT

International Application No PCT/US 86/01934

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) [6]

According to International Patent Classification (IPC) or to both National Classification and IPC

IPC[4]: H 01 P 5/12; H 01 P 1/162

II. FIELDS SEARCHED

Minimum Documentation Searched [7]

Classification System	Classification Symbols
IPC[4]	H 01 P

Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched [8]

III. DOCUMENTS CONSIDERED TO BE RELEVANT [9]

Category *	Citation of Document, [11] with indication, where appropriate, of the relevant passages [12]	Relevant to Claim No. [13]
Y	US, A, 3182326 (C.C. CUTLER) 4 May 1965 see the whole document --	1-3,5-10
A	EP, A, 0020196 (THOMSON-CSF) 10 December 1980, see the abstract; figures 1a,1b; page 2, line 1 - page 4, line 22 --	1
Y	US, A, 2692977 (R.G. KOPPEL) 26 October 1954, see the whole document --	333/228 R 1-3,5-10
Y	US, A, 2593095 (H.B. BREHM) 15 April 1952 see column 3, line 49 - column 5, line 20; figures --	333/122 1-3,5,7-10 81R
A	US, A, 2916659 (T.D. SEGE) 8 December 1959 see column 3, line 54 - column 4, line 22, figures --	1,3,5-7
A	US, A, 2877380 (M. ESTERSON et al.) 10 March 1959, see column 1, line 71 - column 2, line 12; figure 3 --	1,3
A	GB, A, 887572 (MARCONI'S WIRELESS) 17 January 1962, see page 1, ./.	2,8

* Special categories of cited documents: [10]

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

IV. CERTIFICATION

Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report
24th March 1987	7 [illegible] 1987
International Searching Authority	**Signature of Authorized Officer**
EUROPEAN PATENT OFFICE	[illegible] VAN MO[illegible]